# SWIM FM calibration report

SWIM FM calibration report<br>Martin Wieser<br>Swedish Institute of Space Physics, IRF, Kiruna<br>Last compilation: July 2009 Martin Wieser Swedish Institute of Space Physics, IRF, Kiruna

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# Chapter 1

# DRAFT COPY The instrument

# 1.1 Instrument description

Add instrument description here...

## 1.2 Coordinate systems

Description of coordinate systems used in this report here...

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# Chapter 2

# Electrical interface

### 2.1 Conversion functions

**Example 11 Interface**<br> **Example 12 Interface**<br> **IM** conversion functions<br> **IM** conversion functions<br> **IM** conversion functions<br> **IM** conversions internally six separacely controllable high voltages plus one temperature m SWIM contains internally six separately controllable high voltages plus one temperature monitor. Voltages are controlled by references and measured by monitors. There are two sets of conversion functions: a) convert a digital reference value to a predicted voltage, b) convert a digital monitor value to a measured voltage. Both conversions use function of the type

$$
y = ax^2 + bx + c \tag{2.1}
$$

where:

- $a, b$  and  $c$  are tabulated coefficients,
- xthe digital monitor (ADC value) or digital reference (DAC value) and,
- $\bullet$  ythe corresponding value in physical units.

### 2.2 Monitors

Conversion coefficients for digital monitor values are given in Table 2.1. Note that x is always a positive value, independent of the polarity of the voltage in the sensor. The obtained value for  $y$ is also positive independent of the polarity of the real voltage in the sensor.

Monitor name	$\boldsymbol{a}$	b	$\boldsymbol{c}$	Physical unit for $y$	Polarity
Main	0.0	1.3567	$-6.4155$	Volts	$+$ .
<b>CEM</b>	$2.0e-5$	1.2784	0.0	<b>Volts</b>	$\hspace{0.1mm} +$
Defl. upper	0.0	1.2053	$-4.0$	Volts	
Defl. lower	0.0	1.2085	$-4.0$	Volts	
Anyz	0.0	1.1979	$-3.2$	<b>Volts</b>	
Cell	$7.0e-5$	1.1484	8.9559	Volts	
Temp	0.0	0.101725	$-244.08$	$^{\circ}C$	

Table 2.1: Coefficients to convert digital monitor values to physical units

### 2.3 References

Table 2.2 shows coefficients to convert digital reference values to expected physical units. These values should be used if the monitor readings can not be used for any reason. The predicted polarity is always positive independent of the polarity of the voltage in the sensor. If the predicted value for a voltage is negative the result must be treated with caution as depending on temperature the prediction may be invalid.

Table 2.2: Coefficients to convert digital references to predicted voltages

				Table 2.2: Coefficients to convert digital references to predicted voltages	
Reference name	$\boldsymbol{a}$	$\overline{b}$	$\overline{c}$	Physical unit for $y$	Polarity
Main	0.0	15.585	221.56	<b>Volts</b>	$+/-$
$\overline{\text{CEM}}$	$5.0e-4$	16.694	$-144.48$	<b>Volts</b>	$+$
Defl. upper	$-1.0e-6$	1.0201	$-274.71$	<b>Volts</b>	$\blacksquare$
Defl. lower	$-7.0e-7$	1.0191	$-272.26$	<b>Volts</b>	ä,
Anyz	$-4.0e-6$	0.9994	$-251.80$	<b>Volts</b>	ä,
$\overline{\text{Cell}}$	$\overline{0.0}$	5.5277	$-90.340$	<b>Volts</b>	÷,

# Chapter 3

# Sensor properties

### 3.1 Electrostatic analyzer

### 3.1.1 Analyzer constant

The electrostaic analyzer is characterized by the linear function

$$
E/q = k \cdot U_{ESA} \tag{3.1}
$$

with  $E/q$  the particle energy per charge in eV/q,  $U_{ESA}$  the voltage on the ESA plate, and k the analyzer constant.  $k$  was measured at 4 different energies and 3 different angles of incidence. For better noise suppression the ESA voltage was calculated using digital reference values with coefficients taken from Table 2.2. Within the given error, the analyzer constant  $k$  is independent of energy and angle of incidence (" $az$ " in Figure 3.1). The same value for k is valid for start counter and for coincidence events:

$$
k = 4.250 \pm 0.005
$$
 (3.2)



Figure 3.1: Analyzer constant

### 3.1.2 Energy resolution

The width of the energy pass band depends mainly on viewing direction and type of event data used (Figure 3.2). The energy pass band is well approximated by a Gaussian. The FWHM values normalized to energy  $(\Delta E/E)$  are given in Figure 3.2. The energy dependence is less well understood. Measurements below 1 keV have larger errors due to worse counting statistics and larger influence of small voltage offset errors. Weighted averages of  $\Delta E/E$  for the energy range  $100 \text{ eV} - 3000 \text{ eV}$  are given in Table 3.1.





### 3.1.3 Energy table

SWIM uses 32 energy steps (Estep) to cover the energy range under investigation. The energy table used after commissioning is shown in Table 3.2. Due to the double anglular scan (see Chapter 3.2) two consecutive energy steps have the same center energy but different viewing directions.

Table 3.1: Weighted average energy resolution  $\Delta E/E$  for 100 eV = 3000 eV<br>  $\frac{50 \text{ atm}}{50 \text{ atm} \cdot \text{comp}}$  ( $\frac{10}{200 \cdot 10^{-24} \cdot 0.001} = \frac{40}{1000 \cdot 20^{-4} \cdot 0.001} = \frac{40}{1000 \cdot 20^{-4} \cdot 0.001}$ <br>  $\frac{1}{\text{Coincidence counter}} = \frac{0.0702 + 0.00$ 

the same center energy.

Energy step Estep	Center energy [eV]
$\boldsymbol{0}$	109
$\overline{1}$	109
$\overline{2}$	136
$\overline{3}$	136
$\overline{4}$	169
$\overline{5}$	169
$\overline{6}$	210
7	210
$\overline{8}$	262
$\overline{9}$	262
$\overline{10}$	327
$\overline{11}$	327
$\overline{12}$	408
$\overline{13}$	408
14	509
$\overline{15}$	509
$\overline{16}$	636
$\overline{17}$	636
$\overline{18}$	794
$\overline{19}$	794
$\overline{20}$	992
$\overline{21}$	992
$\overline{22}$	1,240
$\overline{23}$	1,240
$\overline{24}$	1,549
$\overline{25}$	1,549
$\overline{26}$	1,935
$\overline{27}$	1,935
$\overline{28}$	2,418
29	2,418
$\overline{30}$	3,022
31	3,022



Figure 3.2: Energy resolution $\Delta E/E$ . Top: using start counter; bottom: using coincidence event data.

### 3.2 Angular pixels

### 3.2.1 Double angular scan

Data processing on the DPU uses in a maximum resolution mode 8 angular pixels and 32 energy steps. To get angular coverage without gaps, 2 consecutive energy steps have the same energy but slightly different angular viewing directions. This allows to simulate a mode with 16 angular pixels and 16 energy steps. Table 3.3 gives the nominal viewing directions for the pixels for two consecutive energy steps. The pattern in Table 3.3 repeats 16 times until all 32 available Estep values are covered. Table 3.4gives the names of the 16 viewing directions obtained with this method.As long as the default maximum resolution mode is used on the DPU, the only impact of the double angular scan is on interpretation of the matrix provided by the DPU. Figure xxx shows how the elements in the accumulation matrix are arranged.

Table 3.3: Nominal SWIM pixel viewing directions in degrees azimuth. Azimuth= -90° points to nadir,  $+90^{\circ}$  points to zenith for nominal s/c attitude. Dstep and Estep numbers refer to the description used in the DPU documentation.

	Dstep							
Estep			D2	D3	D4	$\Box$ D5 $\Box$	D5	
$E_n$ (even numbers)	$-64$	-44	$-25$	-8				
$E_{n+1}(\text{odd numbers})$	$-54$	-34	$-16$				$\mathbb{K}$ 1	

Table 3.4: Naming of SWIM pixel viewing directions. Dstep and Estep numbers refer to the description of deflection and energy steps used in the DPU documentation.



### 3.2.2 Pixel shape

The shape of angular pixels depends on viewing direction. Figure 3.3 shows the shape of a enter looking pixel at azimuth approximately 0°. The shape does not depend much on weather start counters data or coincidence data is used. For calibration, 7 viewing directions (azimuth  $= -64^{\circ}$ , -34°, -16°, 0°, 16°, 34°, 64°) were measured. Pixel shape was then parametrized to obtain the shape for arbitrary intermediate viewing directions.



**Figure 3.3:** Example of angular pixel shape  $(H^+, 1300 \text{ eV})$ . The pixel position corresponds most closely to pixel CH-3H from Table 3.4). X\_pos denotes the azimuth angle in degrees. Y\_pos the elevation angle in degrees. Intensity is normalized to an arbitrary scale, the ratio between the two plots is correct however. The shape of the top pannel is derieved from start events, the bottom pannel from coincidence events. Note the highly nonlinear color scale.

Pixel shape in elevation direction is in first oder independent of the azimuthal viewing direction and is well approximated by a gaussian. In azimuth direction the pixel shape changes depending on viewing direction. The parametrization of the azimuthal shape uses a viewing direction dependent and energy normalized deflection function  $dVE$  as free parameter in analogy to the analyzer constant used for the electrostatic analyzer.

$$
dVE\left(az\right) = \frac{\Delta U_{defl}\left(az\right)}{E_{center}}\tag{3.3}
$$

az denotes the azimuth angle in degrees,  $\Delta U_{def} = U_{deflupper} - U_{deflower}$  the viewing direction dependent voltage difference between the upper and lower deflector electrode in volts, and  $E_{center}$  the center energy selected by the ESA in eV. The value of  $dVE$  is fitted to observed viewing directions using

### 3.2. ANGULAR PIXELS 15

$$
dVE (az) = -0.5078 \cdot \sin \left[ (0.9748 \cdot az + 0.1016) \frac{\pi}{180^{\circ}} \right]
$$
 (3.4)

Pixel shapes  $y(dVE)$  is modelled using an asymetric gauss function:

$$
y(dVE) = max \left(0, A_4 + A_0 \cdot \left\{ \begin{array}{rcl} (dVE - A_1) > 0 & : & e^{-\frac{(x - A_1)^2}{2[A_2(1 - A_3)]^2}} \\ & else & : & e^{-\frac{(x - A_1)^2}{2[A_2(1 + A_3)]^2}} \end{array} \right\} \tag{3.5}
$$

with the  $max(a, b)$  returning the larger of the two values aand b, and  $A_n$  fit parameters. Interpolated fit parameters  $A_n$  for all 16 pixels fron Table 3.4 are shown in Table 3.5, the resulting pixel shapes in Figure 3.5.



Figure 3.4: Collection of parameter sets obtained from tting measured peak shapes. X-axis on all plots is  $dVE$ . The colors indicate three different datasets obtained separately.

### 3.2.3 Flatfield

Flatfield calculations here...

channel	dVE	Ampl. A0	<b>Center A1</b>	Sigma A2	<b>Skew A3</b>	<b>Offset A4</b>
CH-OL	0.4300	0.1220	$-63.0990$	7.4881	0.2357	0.0000
$CH-1L$	0.3400	0.3295	$-46.0450$	5.7444	0.1322	0.0000
CH-2L	0.2100	0.6292	$-27.2737$	3.9193	$-0.0024$	0.0000
CH-3L	0.0700	0.9520	$-9.7369$	2.8705	$-0.1277$	0.0000
$CH-4L$	$-0.0700$	0.7970	7.0870	2.7722	$-0.2325$	0.0000
CH-5L	$-0.2100$	0.5586	24.6238	3.6247	$-0.3169$	0.0000
CH-6L	$-0.3400$	0.3372	43.3951	5.2674	$-0.3770$	0.0000
CH-7L	$-0.4400$	0.1669	62.8364	7.0888	$-0.4112$	0.0000
CH-0H	0.3900	0.2142	$-54.7824$	6.6646	0.1887	0.0000
$CH-1H$	0.2700	0.4909	$-35.4633$	4.6598	0.0575	0.0000
CH-2H	0.1300	0.8137	$-17.0752$	3.2036	$-0.0765$	0.0000
CH-3H	0.0000	0.9162	$-1.3249$	2.7025	$-0.1826$	0.0000
CH-4H	$-0.1300$	0.6948	14.4254	3.0212	$-0.2712$	0.0000
CH-5H	$-0.2700$	0.4564	32.8135	4.2810	$-0.3468$	0.0000
CH-6H	$-0.3900$	0.2520	52.1326	6.1174	$-0.3954$	0.0000
$CH-7H$	$-0.4500$	0.1499	65.4081	7.2976	$-0.4140$	0.0000

Table 3.5: Summary of parameters describing all 16 pixels Parametrisation in azimut direction



Figure 3.5: SWIM pixel shapes in azimutal direction. In elevation direction all pixels are similar and can be modelled by a Gaussian (see Table 3.5). The dotted line is the sum of the response function of all pixels. To obtain a flat response over azimuth, appropriate weighting of each pixel is needed

### 3.3 Mass resolution

Mass resolution here...

### 3.4 Binning

### 3.4.1 Mass calculation and binning

Mass  $m/q$  of a particle is calculated onboard by evaluating

$$
(1 - \eta(m, E_p)) \cdot [E_p + U_{TOF} \cdot e \cdot q] = \frac{1}{2} m m_p v^2
$$
\n(3.6)

(1 –  $\eta(m, E_p)$ ) ·  $|E_p + U_{TOF} \cdot e \cdot q| = \frac{1}{2}m m_p v^2$  (3)<br>
A  $E_p$ the energy of the particle,  $\eta$  the energy loss at the start structure depending on particle and<br>
particle energy,  $U_{TOF}$  the postacceleration the particle e with  $E_p$ the energy of the particle,  $\eta$  the energy loss at the start surface depending on particle mass and particle energy,  $U_{TOF}$  the postacceleration the particle experiences when reaching the TOF section, e the elementary charge,  $m_p$  the proton mass, v the velocity in the TOF section, and m the mass in amu. The calculation does not include any energy loss at various reflecting surfaces for reasons given below. With  $v = \frac{s}{t}$ , where s the path length in the TOF section and t the measured TOF and  $U_P = E_P/(e \cdot q)$ ,  $\sqrt{m/q}$  is obtained by

$$
\sqrt{m/q} = k(U_P) \cdot t = \left[ \sqrt{\frac{2e}{m_p}} \cdot \sqrt{(1 - \eta(m, E_p)) \cdot (U_{TOF} + U_P) e} \cdot s^{-1} \right] \cdot t \tag{3.7}
$$

The factor  $k(U_P)$  is tabulated in the ETOF table. The energy loss  $\eta(m)$  at the start surface is not exactly known. The tabulated value in ETOF therfore assumes  $\eta(m, E) = 0$  for all m and E. This results in a overestimation of  $\sqrt{m/q}$  for large values of  $m/q$ , but removes cumbersome emegy and mass dependency of  $\eta$  form the lookup tables. Table 3.6 shows the parameters used to characterize the TOF cell.

Table 3.6: TOF section properties used to calculate lookup tables

Parameter	Value
Energy loss $\eta$	
TOF cell length $s$	$30 \,\mathrm{mm}$

The mass bin numer M is calculated by mapping  $\sqrt{m/q}$  from Equation 3.7 to 32 mass bins, numbered from 0 to 31:

$$
M = \min\left[\text{floor}\left(\frac{\sqrt{m/q}}{\sqrt{m_{max}}} \cdot 32\right), 31\right]
$$
\n(3.8)

min  $(a, b)$  returns the smaller of two values, floor  $(x)$  rounds down to the lext lower integer number.  $m_{max} = 64$ . The min-function collects all  $m/q > m_{max}$  in the highest mass bin  $M = 31$ . Table 3.7 shows the ideal mass bins.

Note that current flight tables are calculated using an analyzer constant k of 4.255. The current best value for k is 4.250 (see Equation 3.2).

### 3.4.2 TOF peak shapes

Add plots and fit functions for TOF-peak shapes for various  $m/q$  here...

Table 3.7: Ideal mass bin mapping without energy loss on start surface.  $H^+$ will mostly show in mass bin 4 due to energy loss. Bin 31 is a "catch-all" bin for  $m > 60$ amu.

<b>Table 3.7:</b> Ideal mass bin mapping without energy loss on start surface. $H^+$ will mostly show in mass bin 4 due to energy loss. Bin 31 is a "catch-all" bin for $m > 60$ amu.				
	mass bin $M$	from [amu]	to [amu]	
	$\boldsymbol{0}$	0.00	$0.06\,$	
	$\overline{1}$	0.06	0.25	
	$\overline{2}$	0.25	0.56	
	$\overline{3}$	0.56	1.00	
	$\overline{4}$	1.00	1.56	
	$\overline{5}$	1.56	2.25	
	$6\phantom{.}6$	2.25	3.06	
	$\overline{7}$	3.06	4.00	
	$\overline{8}$	4.00	5.06	
	$\overline{9}$	5.06	6.25	
	$\overline{10}$	6.25	7.56	
	$\overline{11}$	7.56	9.00	
	$\overline{12}$	9.00	10.56	
	$\overline{13}$	10.56	12.25	
	14	12.25	14.06	
	$\overline{15}$	14.06	16.00	
	$\overline{16}$	16.00	18.06	
	$\overline{17}$	18.06	$\overline{20.25}$	
	18	$\overline{20.25}$	22.56	
	$\overline{19}$	$\overline{22.56}$	25.00	
	$\overline{20}$	25.00	27.56	
	$\overline{21}$	27.56	30.25	
	$\overline{22}$	30.25	33.06	
	$\overline{23}$	33.06	36.00	
	$\overline{24}$	36.00	39.06	
	$\overline{25}$	39.06	42.25	
	$\overline{26}$	42.25	45.56	
	$\overline{27}$	45.56	49.00	
	$\overline{28}$	49.00	52.56	
	29	52.56	56.25	
	$\overline{30}$	56.25	60.06	
	$\overline{31}$	60.06	inf	

### 3.5 Geometric factor

### 3.5.1 Definitions

The geometrtic factor for a individual pixel is given by

$$
G(n) = G_R(n) \cdot G_0 \tag{3.9}
$$

with  $G_R(n)$ the relative geometric factor of pixel n normalized to  $G_0$ . This is done because ratios of the geometric factor between different pixels can be determined with much higher accuracy than the absolute value.  $G_0$  depends also on the kind of data used: Start-, Stop-, or Coincidence events; whereas  $G_R(n)$  only shows a very weak dependency on the event type.

### 3.5.2 Geometric factor for hydrogen

The relative geometric factor  $G_R^{Start}$  normalized to the CH-3H pixel for 1300eV  $H^+$ for the start counter is shown in Figure 3.6 and Table3.8. The tabulated values are valid for the energy range of 500 eV .. 3000 eV. The values in Table 3.8 does not yet include the slightly higher energy resolution at large deflection angles az. This leads to a slight overestimation ( $\degree$ 10%) of the relative geometric factor for pixels with  $abs(az) > 40^{\circ}$ . The absolute geometric factor  $G_0$  used for normalization depends slightly on energy, with a higher value at lower energies (Table 3.9) . Use Equation 3.9 and values in Table 3.8 to get absolute geometric factors for each pixel for start events.

The absolute geometric factors for coincidence events is obtained by replacing  $G_R^{Start}$  by  $G_R^{Coinc}$ <br>in Equation 3.9. The relative geometric factor  $G_R^{Coinc}$  for coincidence events is approximately given by Equation 3.10. Note that it is important to verify this relation with flight data to get more accuracy.



**Figure 3.6:** Relative geometric factor  $G_R$  for  $H^+$  at 1300 eV versus pixel center direction

Note: When calculating flux, keep the duty cycle of  $1/256$  in mind from energy and deflection sweeping.

### 3.5.3 Other elements

Other elements here...

**Table 3.8:** Geometric factors  $G_R^{Start}$  for start counter and coincidence events for  $H^+$ . The values shown are strictly valid only for 500 eV ... 3000 eV  $H^+$ only, but may be used for a larger energy range at the extent of an additional error.

t the extent of an additional error.			
	Pixel name	relative GF $G_R^{Start}$ for start counter $(1\sigma)$	
	$CH-0L$	$0.33 + 0.1$	
	$CH-1L$	$0.69 \pm 0.1$	
	$CH-2L$	$0.90 \pm 0.1$	
	$CH-3L$	$1.00 \pm 0.1$	
	$CH-4L$	$0.81 \pm 0.1$	
	$CH-5L$	$0.74 + 0.1$	
	$CH-6L$	$0.65 \pm 0.1$	
	$CH-7L$	$0.43 \pm 0.1$	
	$CH-0H$	$0.52 \pm 0.1$	
	$CH-1H$	$0.84 \pm 0.1$	
	$CH-2H$	$0.84 \pm 0.1$	
	$CH-3H$	$0.95 \pm 0.1$	
	$CH-4H$	$0.91 \pm 0.1$	
	$CH-5H$	$0.77 \pm 0.1$	
	$\overline{\text{CH-7H}}$	$0.71 \pm 0.1$	
		Energy ${\cal E}$ $G_0$ $\Omega$	

Energy $E$	$G_0$
[eV]	$\mathrm{cm^2\,sr\,eV/eV}$
500	$+\overline{100\%}$ $5.54{\cdot}10^{-5}$ $-50\%$
1300	$+100\%$ $5.37{\cdot}10^{-5}$ $-50\%$
3000	$+100%$ $4.29{\cdot}10^{-5}$ $-50\%$

**Table 3.9:** Absolute geometric factors  $G_0$  for  $H^+$ . The errors given are a preliminary estimate.